

On the Power Dependence of Extraneous Microwave Fields in Atomic Frequency Standards

S.R. Jefferts, J.H. Shirley, N. Ashby, T.P. Heavner, E.A. Donley
NIST –Time and Frequency Division,
325 Broadway
Boulder , CO USA 80305

F. Levi
Istituto Elettrotecnico Nazionale – Torino IT

ABSTRACT

We show that the frequency bias caused by distributed cavity phase has a strong dependence on microwave power. We also show that frequency biases associated with microwave leakage have distinct signatures in their dependence on microwave power and the physical location of the leakage interaction with the atom.

1. INTRODUCTION

The subject of frequency shifts in atomic frequency standards caused by distributed cavity phase and microwave leakage in the microwave spectrum goes back to the earliest days of the thermal beam standards [1, 2], and has been the subject of continuing theoretical and experimental work over the last fifty years. [3-8]. Laser-cooled fountain frequency standards pose problems with respect to both distributed cavity phase and microwave leakage different from those associated with thermal beam standards. This is due both to the very different microwave structure used in fountains as well as the low center-of-mass velocity and very narrow velocity distribution, which allows operation at significantly elevated microwave power in fountain standards.

We discuss the dependence on microwave power of the frequency biases induced in an atomic fountain by the distributed cavity phase (DCP) and microwave leakage. The entire discussion takes place within the limit of small detuning because the velocity of the atoms, typically a maximum of ~ 3 m/s, results in a maximum Doppler shift of only ~ 100 Hz. We first discussed the power sensitivity of the distributed cavity phase shift (DCPS) in [9], and subsequent work both by our group [10] and the Gibble group at Penn state confirm the existence of a power dependent DCPS [11].

The analysis of the phase of the microwave field within the, typically TE_{011} , microwave cavities used in cold-atom fountain frequency standards has been extensively analyzed. DeMarchi provided the seminal contributions of proving a correspondence between the phase and power-flows within the microwave cavity, identifying the preferred cavity configuration and modeling the phase of the microwave field within the cavity [12-15]. Three-dimensional analyses of the

microwave field within the cavity have been completed by several authors [16-20]. In many of these studies large phase excursions are predicted. At least one author has used these phase excursions to predict frequency shifts in the $\delta f/f \geq 10^{-16}$ range as a result of distributed cavity phase [17], larger than the current value assigned in the error budget of many operational fountain type primary frequency standards. We note that the theory presented here allows one to test that prediction; we have done so and found the prediction of [17] incorrect.

We begin by briefly reviewing the properties of the microwave field within a resonant TE_{011} cavity. We then solve the Schrödinger equation for a two-level atom in the case where the field within the microwave cavity has both real and imaginary parts, which is the case required to understand both the distributed cavity phase frequency shift and the microwave leakage frequency shift. Finally we examine the dependence on microwave field amplitude of the frequency bias caused either by distributed cavity phase or microwave leakage.

2. MICROWAVE CAVITIES AND PHASE

The typical microwave cavity used in cesium (and rubidium) fountain frequency standards is a cylindrical cavity resonating in the TE_{011} mode at the hyperfine frequency of the atom, 9.193 GHz in the case of cesium. See Fig. 1. The “z-axis” of the cavity is aligned with the gradient of the gravitational potential and atoms enter and leave the cavity via below-cutoff waveguides. This cavity has the crucial property of allowing relatively large diameter ($2r_a \sim 1$ cm at $\nu_0 = 9.2$ GHz.) cylindrical waveguides for atoms to enter and leave the cavity without unduly influencing the TE_{011} mode of the cavity and thereby causing large phase gradients in the microwave field [13]. To lowest order the field within the cavity is describable as purely TE ($E_z \equiv 0$) and all field components are derivable from the longitudinal magnetic field $H_z(x,y)$ [13,14]. Under these assumptions, and using a trivial extension of the notation of DeMarchi in [14], the longitudinal field can be written as

Report Documentation Page			Form Approved OMB No. 0704-0188		
Public reporting burden for the collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to a penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.					
1. REPORT DATE AUG 2005		2. REPORT TYPE		3. DATES COVERED 00-00-2005 to 00-00-2005	
4. TITLE AND SUBTITLE On the Power Dependence of Extraneous Microwave Fields in Atomic Frequency Standards			5a. CONTRACT NUMBER		
			5b. GRANT NUMBER		
			5c. PROGRAM ELEMENT NUMBER		
6. AUTHOR(S)			5d. PROJECT NUMBER		
			5e. TASK NUMBER		
			5f. WORK UNIT NUMBER		
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) National Institute of Standards and Technology (NIST), Time and Frequency Division, 325 Broadway, Boulder, CO, 80305			8. PERFORMING ORGANIZATION REPORT NUMBER		
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)			10. SPONSOR/MONITOR'S ACRONYM(S)		
			11. SPONSOR/MONITOR'S REPORT NUMBER(S)		
12. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution unlimited					
13. SUPPLEMENTARY NOTES Joint IEEE International Frequency Symposium and Precise Time and Time Interval (PTTI) Systems and Applications Meeting, 29-31 Aug 2005, Vancouver, BC, Canada					
14. ABSTRACT We show that the frequency bias caused by distributed cavity phase has a strong dependence on microwave power. We also show that frequency biases associated with microwave leakage have distinct signatures in their dependence on microwave power and the physical location of the leakage interaction with the atom.					
15. SUBJECT TERMS					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT Same as Report (SAR)	18. NUMBER OF PAGES 6	19a. NAME OF RESPONSIBLE PERSON
a. REPORT unclassified	b. ABSTRACT unclassified	c. THIS PAGE unclassified			

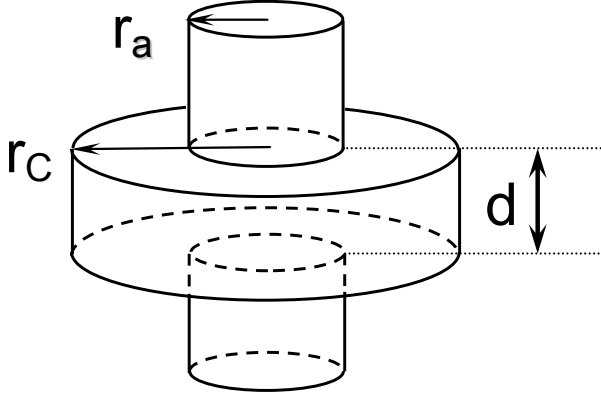


Figure 1. A schematic diagram of the TE_{011} microwave cavity used in most cesium fountain frequency standards.

$$H_z(x, y, z) = |H(x, y)| e^{i\varphi(x, y)} f(z) \hat{z}, \quad (1)$$

where $\varphi(x, y)$ is the distributed cavity phase under discussion here. The expression for the real part of the field within the cavity is given (with a change to cylindrical coordinates ρ, ϕ and z) to lowest order by

$$\begin{aligned} \text{Re}(H_z(\rho, \phi, z)) \approx & A_{0,1,1} \left(\frac{\pi}{2} \right) H_0 J_0 \left(\frac{p'_{0,1} \rho}{r_c} \right) \sin \left(\frac{\pi z}{d} \right) + \\ & \sum A_{n,m,l} J_n \left(\frac{p'_{n,m} \rho}{r_c} \right) e^{\pm i n \phi} \sin \left(\frac{l \pi z}{d} \right), \end{aligned} \quad (2)$$

where J_n is the n^{th} Bessel function and $p'_{n,m}$ is defined as

the m^{th} solution of $\frac{dJ_n(x)}{dx} = 0$, r_c is the radius of the

cavity and d is the height of the cavity (see Fig. 1 and [21]). The first term is the desired TE_{011} fundamental mode of the cavity, while the infinite sum of higher order modes with coefficients $A_{n,m,l}$ comes from the required cavity imperfections, especially the apertures on the end caps, which allow atoms to enter and exit the cavity, and the feed apertures or antennas that couple power into the cavity. The cavity phase is defined by the relation

$$\varphi \equiv \tan^{-1} \left(\frac{\text{Im}(H_z)}{\text{Re}(H_z)} \right), \quad (3)$$

where the real part of H is approximated by Eq (2), or to a reasonable approximation that allows for an analytic result the real part of H as approximated by the first term in Eq. (2). The imaginary part of the field is a result of losses within the cavity, primarily ohmic losses of the surface currents on the cavity walls. Whatever the details of the imaginary part of the field, it can be expanded as an infinite sum of $TE_{n,m,l}$ modes that provide a set of basis functions [19,21].

Thus

$$\text{Im } H_z \propto \sum_{n,m,l} B_{n,m,l} J_n \left(\frac{p_{n,m} r}{r_c + \delta} \right) e^{\pm i n \phi} \sin \left(\frac{l \pi z}{d + 2\delta} \right), \quad (4)$$

where δ is the skin depth inside the cavity. Higher order azimuthal ($n > 0$) modes are excited by the feed structure of the cavity, while higher order radial ($m > 1$) modes and higher order longitudinal modes ($l > 1$) are excited by the cavity apertures as well as construction imperfections [21]. The coefficients $A_{n,m,l}$ and $B_{n,m,l}$ for $l=2,4,\dots,2n$ should be quite small for a cavity with mid-plane feeds; however, this may not be true for the “improved” cavity design described in [20]. Additionally with mid-plane fed cavities the predominant power flow caused by coupling imbalance is orthogonal to the atomic trajectory, resulting in a high degree of rejection of the first order Doppler shift; this feature is lost in cavities not using the midplane feed such as those in [20], which exhibit a high sensitivity to first order Doppler shifts.

Several things can be seen by inspection of the previous equations. First, the phase of the microwave field within the cavity is independent of microwave power (as it should be). Second, the microwave phase can become relatively large when the real part of H_z is sufficiently small, or equivalently, the Rabi frequency of the atom is sufficiently small. What is ultimately of interest, of course, is not the value of the phase angle of the microwave field, but rather the value of the phase angle imposed on the atomic wave function as a result. The effect on the atom of the imaginary part of H_z is dependent on the microwave power, in spite of the phase of the microwave field being independent of that same power.

We have previously expanded the imaginary part of the field using a power series [22,15], which results in an expression such as

$$\text{Im}(H_z) = \frac{\pi H_0}{2Q} \left[\frac{\left(\sum \left(\frac{r}{r_c} \right)^n (A_n + B_n \cos n\phi) \right)}{\sum C_m \left(\frac{z}{d} - \frac{1}{2} \right)^m} \right], \quad (5)$$

where again the odd terms in the series are small as a result of symmetry considerations. The Penn State group has obtained similar but more complete power series expansions [20]. The expansion of the field in terms of a normal mode picture (Eq. (4)) or a power series (Eq. (5)) yields similar power sensitivities of the frequency bias.

In order to quantify the effect of the imaginary part of the microwave field upon the atom, we now obtain a solution to the time-dependent Schrödinger equation as the atoms pass through a cavity with fields described by Eq. (2), (4) & (5).

3. SCHRÖDINGER EQUATION AND RAMSEY LINESHAPES

We extensively employ the theoretical framework developed by Shirley et al. [23-25] and present here the extensions required to handle both the real and imaginary phases of microwave field. The Hamiltonian for the system can be written as (cf. (7) of [25])

$$\mathcal{H} = \hbar \begin{pmatrix} \omega_a & 2b \cos \omega t + 2b' \sin \omega t \\ 2b \cos \omega t + 2b' \sin \omega t & \omega_b \end{pmatrix}, \quad (6)$$

where $\hbar\omega_a$ and $\hbar\omega_b$ are respectively the energies of the upper and lower states. The interaction Rabi frequency for the real part of the microwave field is given by $2b = \mu_B g \text{Re}(H_z)/\hbar$, where μ_B is the Bohr magneton, g the Landé g-factor and H_z the microwave magnetic field parallel to the quantization axis imposed by the external c-field. A similar expression applies for b' , $2b' = \mu_B g \text{Im}(H_z)/\hbar$, the Rabi frequency due to the imaginary part of the microwave field. Both $b(t)$ and $b'(t)$ are time-dependent, owing to the atoms motion in the cavity.

In the rotating wave approximation, the Hamiltonian in Eq. (6) is written

$$\mathcal{H} = \hbar \begin{pmatrix} \omega_a & (b + ib')e^{-i\omega t} \\ (b - ib')e^{i\omega t} & \omega_b \end{pmatrix}. \quad (7)$$

Note the sign change in $b'(t)$ in the off-diagonal couplings. This comes about because the rotating wave approximation selects one exponential from $\sin \omega t$ in one coupling and the other exponential in the other coupling (Compare to (7) and (8) in [21]). Using the “phase factored” solutions, α and β , (cf (9 & 10) of [24]) gives us, finally, the Schrödinger equation for the system,

$$i\hbar \frac{d}{dt} \begin{pmatrix} \alpha \\ \beta \end{pmatrix} = \hbar \begin{pmatrix} -\Delta & b + ib' \\ b - ib' & \Delta \end{pmatrix} \begin{pmatrix} \alpha \\ \beta \end{pmatrix}. \quad (8)$$

With the initial condition $\alpha(0) = 1$ and $\beta(0) = 0$, α is the probability amplitude that the system remains in its initial state and β the probability amplitude that the system changes state. Δ is half the detuning $\delta\omega$ from the atomic resonance ω_0 : $\Delta = \frac{1}{2}(\omega - \omega_0) = \frac{\delta\omega}{2}$,

where $\omega_0 = \omega_a - \omega_b$ is the hyperfine splitting of the atom. Δ , b , and b' are all real, possibly time-dependent, quantities.

We have given a solution to (8), valid through first order in Δ and b' , under the assumption that the detuning is small compared to the Rabi frequency, in [9]. We quote here only the final results.

Using our solutions mentioned above and assuming that the real part of the excitation is the same for both Ramsey pulses leads to a transition probability of

$$P = \frac{\sin^2(2b_0\tau)}{2} \left[1 + \cos \delta\omega T_R + \left\{ (\varepsilon_2 - \varepsilon_1) \csc b_0\tau + \left\{ (\eta_1 + \eta_2) \sec b_0\tau \right\} \sin \delta\omega T_R \right\} \right]. \quad (9)$$

b_0 is defined by $b_0\tau = \int_0^\tau b(t)dt$, that is, b_0 is the average value of $b(t)$ during the excitation time τ , which amounts to $\pi/4$ at optimum power, and $\varepsilon_{1,2}$ and $\eta_{1,2}$ are proportional to the imaginary part of the microwave field b' ; the subscripts refer to the first and second passage through the Ramsey cavity. That is,

$$\eta = b_0\tau \int_0^\tau b'(t) \cos\left(\frac{\pi t}{\tau}\right) dt, \quad (10)$$

$$\varepsilon = b_0\tau \int_0^\tau b'(t) \cos\left(\frac{\pi t}{\tau}\right) dt.$$

From Eq. (9) the transition probability, P , is clearly a normal Ramsey fringe (the $\cos \delta\omega T_R$ term) plus an underlying fringe of small amplitude and $\pi/2$ displacement (the $\sin \delta\omega T_R$ term). The latter asymmetrically distorts the Ramsey curve and leads to a frequency bias. The frequency bias is proportional to the difference between the transition probabilities P_L and P_R on the left and right sides of the central Ramsey fringe at equal detunings. This difference is given by

$$P_L - P_R = \sin^2(2b_0\tau) \left[\frac{\varepsilon_2 - \varepsilon_1}{\sin(b_0\tau)} + \frac{\eta_2 + \eta_1}{\cos(b_0\tau)} \right], \quad (11)$$

where $P_{L,R}$ is the probability given by (9) on the left and right sides of the central Ramsey fringe, respectively (that is with $\delta\omega = \mp \pi/2T_R$, respectively). Eq (11) is plotted below in Fig 2. The complicated nature of the power dependence of the frequency bias associated with distributed cavity phase is immediately apparent in Fig. 2. This signature should allow measurement of the frequency bias associated with distributed cavity phase, or at least allow the placing of an upper limit on the effect.

Two points should be stressed here: First, as noted in our earlier work [9], a power dependence of the DCPS induced frequency bias occurs whenever the curvature of the real and imaginary parts of the field are different over the atomic trajectory. This is bound to occur in any real fountain cavity, which must have apertures in the end caps for the atoms to enter and leave. Second, a frequency shift can only be introduced by a field in quadrature to the principal part of the field (that is, the imaginary part of the field). Variations in the real part of the field cannot lead to a frequency shift in and of themselves.

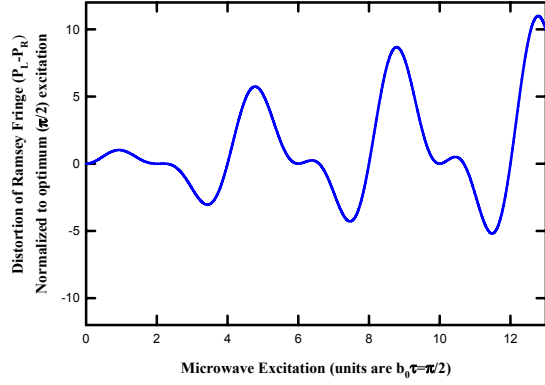


Figure 2. The distortion of the Ramsey fringe plotted caused by distributed cavity phase with respect to the microwave excitation (number of $\pi/2$ pulses). The distortion is proportional to the frequency bias and the data shown here are normalized to the shift at optimum power (one $\pi/2$ pulse).

4. MICROWAVE LEAKAGE

Microwave leakage induced frequency biases have previously been investigated by several authors [6,7]. Because the earlier work was primarily in the context of thermal beam clocks operation at optimum power was investigated and the power sensitivity of the effect was not elucidated. Here, because we are primarily interested in the effects of microwave leakage in the context of fountain frequency standards, we investigate the effect in the context of small detuning (small Doppler shift) and large microwave power.

We can use the Hamiltonian, Eq. (7), also to investigate microwave leakage, except that in this case both b and b' are presumably small. We divide our analysis into three cases: leakage before the two Ramsey interactions, leakage between the Ramsey pulses, and leakage after the Ramsey interactions. Because the state-selection mechanism in NIST-F1 and IEN-CSF1 destroys any microwave coherence and projects the atoms into a pure $F=3$ state we can ignore the case of leakage before the first Ramsey interaction. We note however that the solution to the case of leakage before the first Ramsey interaction can be obtained from the case of leakage after the second Ramsey interaction by the substitution of $-t$ for t .

Some general results can be obtained [26]:

1. Microwave leakage in phase (the b term) with the field in the Ramsey cavity does not (indeed cannot) cause a frequency shift.
2. Microwave leakage in quadrature phase (the b' term) does not cause a frequency shift if it is applied symmetrically with respect to the center of the Ramsey interaction at $T_R/2$.

3. Microwave leakage in quadrature phase applied asymmetrically with respect to $T_R/2$ excites a Ramsey fringe shifted with respect to the central fringe (a $\sin(\delta\omega T_R)$ term) much like that in Eq. (9), which can cause a frequency bias.

We investigate the power dependence of these frequency biases next. Full solutions to the Schrödinger Equation for all three leakage cases are given in [26]. Below the various specific cases of microwave leakage are examined.

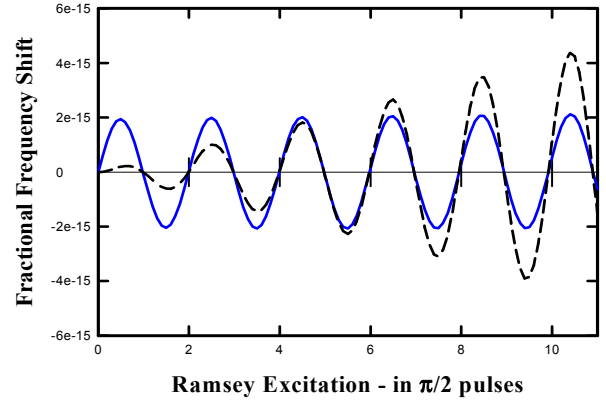


Figure 3. The modeled frequency shift induced by leakage above the Ramsey cavity in NIST-F1 and IEN-CSF1. The solid curve is the case where the leakage amplitude is constant while the field in the Ramsey cavity is increased. The broken curve is the case where the leakage field amplitude is proportional to the amplitude of the field within the Ramsey cavity. The microwave leakage power of each curve was chosen for convenience and has no particular significance.

5. MICROWAVE LEAKAGE BETWEEN THE TWO RAMSEY PULSES

The dependence of the frequency bias on the amplitude of the microwave field in the Ramsey cavity is shown in Fig 3. It is immediately apparent that the frequency bias caused by microwave leakage is zero at integer multiples of the optimum excitation amplitude,

$$b_0\tau = (2n+1)\frac{\pi}{2}, \quad n=0,1,2,\dots$$

The residual frequency bias can be measured with some leverage by measuring well away from optimum power, as illustrated in Fig. 4. In NIST-F1 the microwave power is set to within ± 0.1 dB of optimum, denoted by the dotted lines in Fig. 4. The frequency shift induced by microwave leakage at ± 3 dB from optimum excitation is some 30 times greater than the shift expected within 0.1 dB of optimum. The measurement at ± 3 dB therefore gives a “leverage” of 30 over the standard operating conditions, at least for the specific case of leakage above the Ramsey cavity.

7. DISCUSSION

The frequency biases caused by distributed cavity phase and microwave leakage have distinct signatures when measured as a function of the amplitude of the microwave excitation in the Ramsey cavity. The various shifts can be measured and either “fixed” by eliminating the source of the leakage (best), or perhaps calibrated and corrected.

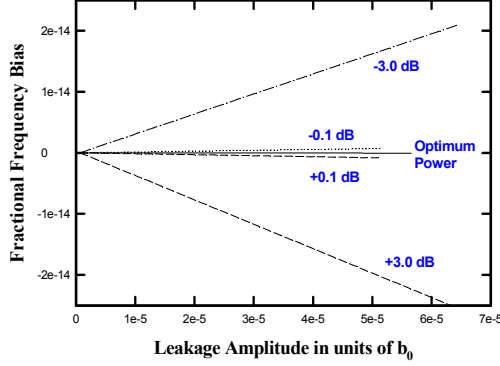


Figure 4. The frequency bias from microwave leakage above the Ramsey cavity can be measured in a “leveraged” fashion by operating well away from optimum microwave power in the Ramsey cavity. Assuming that the normal operating conditions keep the microwave power within 0.1 dB of optimum, a leverage of about 30 can be obtained by operating 3 dB above or below optimum instead.

6. MICROWAVE LEAKAGE AFTER THE RAMSEY INTERACTION

In the case of both NIST-F1 and IEN-CSF1 this is the most likely location for microwave leakage to interact with cesium atoms. The power dependence of this shift is shown in Fig. 5. The behavior of this shift is distinct from that caused by leakage above the Ramsey cavity in that its frequency with respect to the Rabi frequency is half that of the case of leakage above the Ramsey cavity. This signature can be used to identify the source of a frequency bias as being caused by leakage either above or below the Ramsey cavity. Unfortunately this shift is difficult to distinguish from the frequency shift caused by distributed cavity phase, as shown in Fig. 6. Various approaches to separate these two effects are discussed in [26].

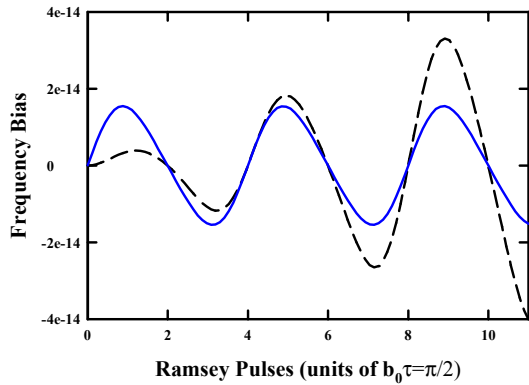


Figure 5. The modeled frequency bias induced by leakage below the Ramsey cavity. The solid curve is the case where the leakage amplitude is constant while the field in the Ramsey cavity is increased. The broken curve is the case where the leakage field amplitude is proportional to the amplitude of the field within the Ramsey cavity. In both cases the microwave power level has been chosen purely for convenience and has no particular significance.

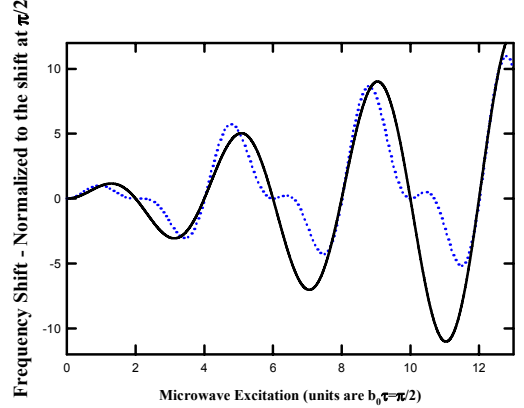


Figure 6. A comparison of the power dependence of the shift caused by microwave leakage (dotted curve) and the shift caused by microwave leakage below the Ramsey cavity (solid curve) as a function of the microwave excitation of the atoms in the Ramsey cavity.

It has been assumed here that the leakage terms can be treated in the small detuning limit. Various other approaches such as using the nonresonant AC Stark shift have been applied to the case of microwave leakage in a cesium fountain [27]. We hold that these cases are not valid approximations in a cesium fountain; the Doppler shift caused by atomic motion is, at 100 Hz maximum, much too small to be considered within the framework of an off-resonant AC Stark shift. The frequency shift caused by microwave leakage in a fountain depends on the amplitude of the microwave field and not on the power (square of the amplitude).

ACKNOWLEDGEMENTS

The authors gratefully acknowledge many useful discussions of microwave field effects in primary frequency standards with Andrea DeMarchi, Bob Drullinger, Bill Klipstein, Stefania Romisch and Tom Parker. We also thank David Smith, Mike Lombardi Tom Parker, Tom O’Brian and Marc Weiss for their many useful suggestions on the manuscript.

Contribution of the U.S. government, not subject to U.S. copyright.

REFERENCES

- [1] N. Ramsey, Molecular Beams, Oxford – Clarendon Press 1956.
- [2] R.C. Mockler, “*Atomic Beam Frequency Standards*”, Adv. Electron El. Phys., **15** (1962) pp.1-72.
- [3] S. Jarvis Jr., “Molecular Beam Tube Frequency Biases due to Distributed Cavity Phase Variations”, NBS Tech. Note 660 (1975).
- [4] A. DeMarchi, J.H. Shirley, D.J. Glaze, and R.E. Drullinger, “*A New Cavity Configuration for Cesium Beam Primary Frequency Standards*”, IEEE Trans. Instrum. Meas. **37** (1988) pp. 185-190.
- [5] A. Bauch, B. Fischer, T. Heindorff and R. Schröder, “Performance of the PTB reconstructed primary clock CS1 and an estimate of its current uncertainty”, Metrologia **35** (1998) pp. 829-845.
- [6] K. Dorenwendt and A. Bauch, “Spurious Microwave Fields in Caesium Atomic Beam Standards: Symmetry Considerations and Model Calculations”, Proc. EFTF, 1999.
- [7] B. Boussert, G. Théobald, P. Cérez and E. deClercq, “*Frequency Shifts in Cesium Beam Clocks Induced by Microwave Leakages*”, IEEE Trans. UFFC **45** (1998) 728-738.
- [8] M. Abgrall, “Evaluation des Performances de la Fontaine Atomique PHARO, Participation à l’étude l’horloge spatiale PHARO”, PhD Thesis, University de Paris VI, January 2003.
- [9] S.R. Jefferts, J.H. Shirley, N. Ashby, E.A. Burt, G.J. Dick, “*Power Dependence of Distributed Cavity Phase Induced Frequency Biases in Atomic Fountain Frequency Standards*”, IEEE Trans UFFC, in press (submitted 31Aug2004).
- [10] S.R. Jefferts et al, Proc of the EFTF 2005 – in press.
- [11] Ruoxin Li, Kurt Gibble, Proc of the EFTF 2005 – in press.
- [12] A. DeMarchi, “The Optically Pumped Caesium Fountain: 10^{-15} Frequency Accuracy?”, Metrologia **18** (1982) pp. 103-116.
- [13] G. Vecchi, A. DeMarchi, “Spatial Phase Variations in a TE₀₁₁ Microwave Cavity for use in a Cesium Fountain Primary Frequency Standard”, IEEE Trans. Instrum. Meas. **42** (1993) pp. 434-438.
- [14] A Khursheed, G. Vecchi, A. DeMarchi, “*Spatial Variations of Field Polarization in Microwave Cavities: Application to the Cesium Fountain Cavity*”, IEEE Trans UFFC. **43** (1996) pp. 201-210.
- [15] S.R. Jefferts, R.E. Drullinger and A. DeMarchi, “*NIST Cesium Fountain Microwave Cavities*”, Proc. 1998 Intl. Freq. Cont. Symp. pp. 6-8.
- [16] P. Laurent et al., “*Interrogation of Cold Atoms in a Primary Frequency Standard*”, Proc. 1999 EFTF Conf. pp. 152-155.
- [17] C. Fertig, R. Li, J. Rees, K. Gibble, “Distributed Cavity Phase Shifts and Microwave Photon Recoils”, Proc. 2002 IEEE Intl. Freq. Cont. Symp. pp. 469-472.
- [18] G.J. Dick, W.M. Klipstein, T.P. Heavner, S.R. Jefferts, “Design Concept for the Microwave Interrogation Structure in PARCS”, Proc. 2003 EEE Intl. Freq. Cont. Symp. pp. 1032-1036.
- [19] N. Ashby, S. Römisch, S.R. Jefferts, “*Endcaps for TE₀₁₁ Cavities in Fountain Frequency Standards*”, Proc. 2003 IEEE Intl. Freq. Cont. Symp pp. 1076-1083.
- [20] Ruoxin Li, Kurt Gibble, “*Phase Variations in Microwave Cavities for Atomic Clocks*”, Metrologia **41** (2004) pp 376-386.
- [21] Robert E. Collin, Foundations of Microwave Engineering, 2nd Ed., McGraw-Hill 1998.
- [22] S.R. Jefferts et al, “*Accuracy Evaluation of NIST-F1*”, Metrologia **39**(2002) pp321-336
- [23] J.H. Shirley, “*Some Causes of Resonant Frequency Shifts in Atomic Beam Machines I. Shifts Due to Other Frequencies of Excitation*”, J. Appl. Phys. **34** (1963) pp.783-788.
- [24] J.H. Shirley, “*Solution of the Schrödinger Equation with a Hamiltonian Periodic in Time*”, Phys. Rev. **138** (1965) pp. B979-B987.
- [25] J.H. Shirley, W.D. Lee, R.E. Drullinger, “*Accuracy Evaluation of the Frequency Standard NIST-7*”, Metrologia **38** (2001) pp. 427-458.
- [26] F. Levi, J. Shirley, S.R. Jefferts, *Microwave Leakage Induced Frequency Shifts in the Primary Frequency Standards NIST-F1 and IEN-CSF1, submitted to IEEE Trans UFFC.*
- [27] K. Szymaniec, W. Chalupczak, P.B. Whibberley, S.N. Lea, D. Henderson, *Evaluation of the Primary Frequency Standard NPL_CsF1*, Metrologia **42** (2005) pp. 49-57.